

Advanced Building Science

- Cooling Load Calculations
 - Principles & considerations
 - Heat flow rates and design conditions
 - Generalized procedures
 - Residential (simplified approach)

- Readings
 - HF - Chapter 17 => primary focus
 - HF - Chapter 18 => (review for procedures and tables)

Cooling Load Calculations

Principles and Considerations

- “Worst case” design loads for the equipment
 - may be different than “worst case” for a specific space
 - room by room calculation is strongly recommended
 - however, peak load may or may not coincide with the largest heat gain for a specific space or the whole house

Cooling Load Calculations

Principles and Considerations

- Far more complicated than heating design loads
 - additional gains
 - solar gain is extremely dynamic and time dependent
 - latent effects probably can't be ignored
 - radiant gains are significant and not always instantaneous
- Timing is everything

Heat Flow/Gain Rates – The Big Picture

- Space heat gain
 - mode of entry
 - sensible or latent heat gain
- Space cooling load
 - radiant heat gain
- Space heat extraction rate
- Distribution gains
- Cooling coil load

Initial Design Conditions

- Building characteristics
- Configuration
 - orientation will be important
- Outdoor design conditions
- Indoor design conditions
- Operating schedules
- Date and time of peak conditions
 - may require a several iterations

Heat Sources and Heat Gain Concepts

- Time delay
- People
- Lighting
- Motors
- Appliances
- Fenestration
- Exterior (and interior) surfaces
- Infiltration & ventilation
- Miscellaneous

It's All About the Heat Balance

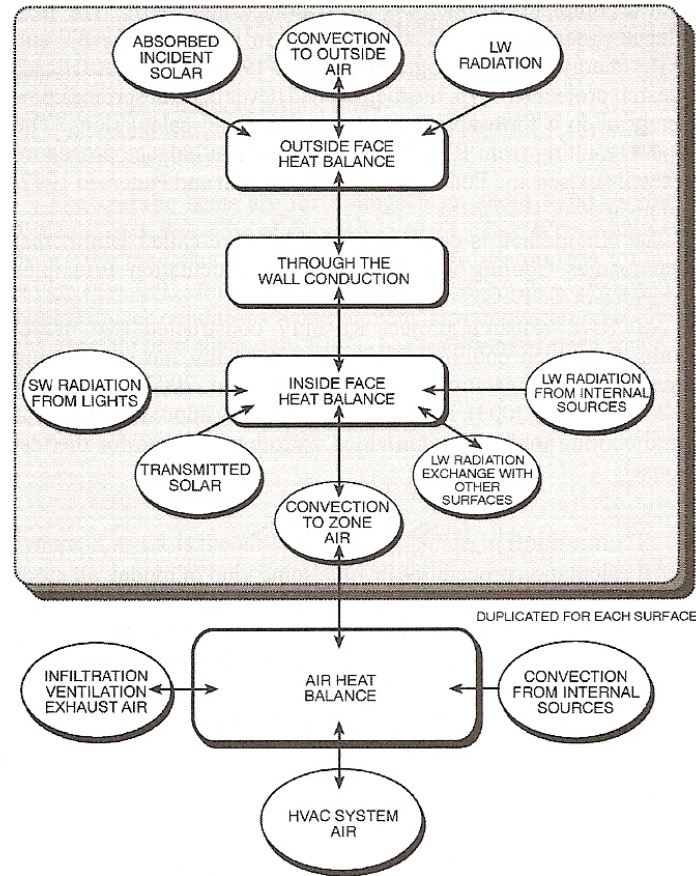


Fig. 5 Schematic of Heat Balance Processes in Zone

Source: ASHRAE Handbook Fundamentals 2013, Chapter 18.15

Overall Cooling Load Methods

Heat Balance (HB) Method

- Assumes well mixed
- Uniform surface temperatures and radiation
- Residential => Residential Load Factor (RLF) Method
 - Basis is ResHB
 - Functionally driven with Cooling Factors
 - See Table 1
- Commercial => Radiant Time Series (RTS) Method
 - Replaces earlier approaches such as
 - transfer function
 - total equivalent temperature difference / time averaging
 - cooling load temperature difference / cooling load factor

Residential Cooling Load Procedure

Unique features

- considered occupied 24 hours per day, every day
- loads are primarily through the structural components
 - comparatively the internal gains are small
- most residences are a single zone
- greater distribution losses (as fraction of total)
- residential cooling units are generally small
- dehumidification only occurs during cooling

Note: Multifamily buildings may or may not fit single family methods depending on exposures and systems used.

General Guidelines

- Design for Typical Building Use
 - Meet representative maximum conditions, not extreme conditions
- Building Codes and Standards
 - Codes and local regulations take precedence
- Design Judgment

General Guidelines

- Verification
 - Post-construction commissioning and verification is important
- Uncertainty & Safety Allowances
 - Due to the general and approximate nature, it may be tempting to add safety allowances for each aspect of the calculation
 - This can be compounding, so allowances (if applied, at all) should be added to final results

Total Sensible Cooling Load

- Heat gain through structural components
 - Below grade is ignored (or considered highly insulated)
- Heat gain through windows
 - transmission
 - solar radiation
- Heat gain caused by air infiltration and ventilation
- Heat gain due to occupancy
- Heat gain due to household equipment
- Heat gain in air distribution system

Latent Cooling Load

- Usually are evaluated separately
- However, for residential buildings they are frequently estimated as a percentage of sensible loads
 - This is clearly flawed, but better than nothing at all
 - Momentum is building to address latent loads more intentionally

Loads Through Opaque Surfaces

- RLF Method uses:

$$q_{\text{opq}} = A \times CF_{\text{opq}}$$

$$CF_{\text{opq}} = U(OF_t \times \Delta T + OF_b + OF_r \times DR)$$

- For ceilings/roof, walls, floors over ambient
 - use “opaque surface cooling factor coefficients”
 - see Table 7 & 8

May reduce load slightly using slab floor procedure

Source: ASHRAE Handbook Fundamentals 2013, Chapter 17.2

Table 7 Opaque Surface Cooling Factor Coefficients

| Surface Type | OF_t | $OF_b, ^\circ\text{F}$ | OF_r |
|---|--------|-----------------------------|--------|
| Ceiling or wall adjacent to vented attic | 0.62 | $25.7 \alpha_{roof} - 8.1$ | -0.19 |
| Ceiling/roof assembly | 1 | $68.9 \alpha_{roof} - 12.6$ | -0.36 |
| Wall (wood frame) or door with solar exposure | 1 | 14.8 | -0.36 |
| Wall (wood frame) or door (shaded) | 1 | 0 | -0.36 |
| Floor over ambient | 1 | 0 | -0.06 |
| Floor over crawlspace | 0.33 | 0 | -0.28 |
| Slab floor (see Slab Floor section) | | | |

α_{roof} = roof solar absorptance (see Table 8)

Source: ASHRAE Handbook Fundamentals 2013, Chapter 17.9

Table 8 Roof Solar Absorptance α_{roof}

| Material | Color | | | |
|---------------------|--------------|--------------|---------------|-------------|
| | White | Light | Medium | Dark |
| Asphalt shingles | 0.75 | 0.75 | 0.85 | 0.92 |
| Tile | 0.30 | 0.40 | 0.80 | 0.80 |
| Metal | 0.35 | 0.50 | 0.70 | 0.90 |
| Elastomeric coating | 0.30 | | | |

Source: Summarized from Parker et al. 2000

Source: ASHRAE Handbook Fundamentals 2013, Chapter 17.8

Loads Through Transparent Surfaces

- RLF Method Uses:

$$q_{fen} = A \times CF_{fen}$$

$$CF_{fen} = U(\Delta T - 0.46DR) + PXI \times SHGC \times IAC \times FF$$

$$PXI = T_x \times E_t \quad (\text{if unshaded})$$

$$PXI = T [E_d + (1 - F_{shd}) E_D] \quad (\text{if shaded})$$

- PXI = Peak Exterior Irradiance [see Table 10, 11, & 12]
- SHGC = solar heat gain coefficient see [Tables or NFRC value]
- IAC = Interior shading attenuation coefficient [see Table 14]
- FF = fenestration solar load factor [see Table 13]

Source: ASHRAE Handbook Fundamentals 2013, Chapter 17.9-11

Table 10 Peak Irradiance, Btu/h·ft²

| Exposure | | Latitude | | | | | | | | |
|---------------------|-------|----------|-----|-----|-----|-----|-----|-----|-----|-----|
| | | 20° | 25° | 30° | 35° | 40° | 45° | 50° | 55° | 60° |
| North | E_D | 40 | 34 | 29 | 26 | 26 | 27 | 30 | 36 | 43 |
| | E_d | 41 | 36 | 33 | 30 | 27 | 24 | 22 | 20 | 18 |
| | E_t | 80 | 70 | 62 | 56 | 53 | 51 | 52 | 55 | 61 |
| Northeast/Northwest | E_D | 146 | 142 | 139 | 135 | 131 | 127 | 122 | 118 | 114 |
| | E_d | 56 | 54 | 51 | 50 | 48 | 47 | 45 | 44 | 43 |
| | E_t | 202 | 196 | 190 | 184 | 179 | 173 | 168 | 163 | 158 |
| East/West | E_D | 168 | 172 | 175 | 177 | 178 | 177 | 176 | 173 | 170 |
| | E_d | 63 | 62 | 61 | 60 | 60 | 60 | 59 | 59 | 59 |
| | E_t | 231 | 234 | 236 | 237 | 237 | 237 | 235 | 233 | 230 |
| Southeast/Southwest | E_D | 89 | 104 | 117 | 128 | 138 | 147 | 154 | 160 | 164 |
| | E_d | 65 | 64 | 64 | 65 | 65 | 66 | 66 | 67 | 68 |
| | E_t | 154 | 168 | 181 | 193 | 203 | 213 | 220 | 227 | 232 |
| South | E_D | 0 | 19 | 44 | 68 | 90 | 110 | 129 | 147 | 163 |
| | E_d | 53 | 61 | 62 | 63 | 65 | 66 | 68 | 70 | 71 |
| | E_t | 53 | 80 | 106 | 131 | 155 | 177 | 197 | 217 | 235 |
| Horizontal | E_D | 268 | 266 | 262 | 255 | 246 | 234 | 219 | 202 | 182 |
| | E_d | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 |
| | E_t | 322 | 320 | 316 | 309 | 300 | 288 | 273 | 256 | 236 |

Source: ASHRAE Handbook Fundamentals 2013
Chapter 17.9

Table 11 Exterior Attachment Transmission

| Attachment | T_x |
|------------------------|---|
| None | 1.0 |
| Exterior insect screen | 0.64 (see Chapter 15, Table 13G) |
| Shade screen | Manufacturer shading coefficient (SC) value, typically 0.4 to 0.6 |

Source: ASHRAE Handbook Fundamentals 2013, Chapter 17.10

Table 14 Interior Attenuation Coefficients (IAC_{cl})

| Glazing Layers | Glazing Type (ID*) | Drapes | | | Roller Shades | | | Blinds | |
|----------------|------------------------|------------|--------------|-------|---------------|-------|-------------|--------|-------|
| | | Open-Weave | Closed-Weave | | Opaque | | Translucent | Medium | White |
| | | Light | Dark | Light | Dark | White | Light | | |
| 1 | Clear (1a) | 0.64 | 0.71 | 0.45 | 0.64 | 0.34 | 0.44 | 0.74 | 0.66 |
| | Heat absorbing (1c) | 0.68 | 0.72 | 0.50 | 0.67 | 0.40 | 0.49 | 0.76 | 0.69 |
| 2 | Clear (5a) | 0.72 | 0.81 | 0.57 | 0.76 | 0.48 | 0.55 | 0.82 | 0.74 |
| | Low-e high-solar (17c) | 0.76 | 0.86 | 0.64 | 0.82 | 0.57 | 0.62 | 0.86 | 0.79 |
| | Low-e low-solar (25a) | 0.79 | 0.88 | 0.68 | 0.85 | 0.60 | 0.66 | 0.88 | 0.82 |
| | Heat absorbing (5c) | 0.73 | 0.82 | 0.59 | 0.77 | 0.51 | 0.58 | 0.83 | 0.76 |

*Chapter 15 glazing identifier

Source: ASHRAE Handbook Fundamentals 2013, Chapter 17.11

Loads Due to Infiltration & Ventilation

- Find air flow and use equations:

$$q_s = C_s \times Q \times \Delta T$$

$$q_l = C_l \times Q \times \Delta W$$

- Air flow

- use procedures Chapter 16 or
- use simplified methods based on effective leakage area and infiltration driving force [see Tables 3, 4, & 5]

$$Q_i = A_l \times IDF$$

Source: ASHRAE Handbook Fundamentals 2013, Chapter 16

Loads Due to Internal Gains

- Use equations:

$$q_{ig,s} = 464 + 0.7A_{cf} + 75N_{oc}$$

$$q_{ig,l} = 68 + 0.7A_{cf} + 41N_{oc}$$

- A_{cf} = conditioned floor area
- N_{oc} = number of occupants

Source: ASHRAE Handbook Fundamentals 2013, Chapter 16

Loads Due to Air Distribution System

- Use equation:

$$q_d = F_{dl} \times q_{bl}$$

- F_{dl} = duct gain factor [see Table 6]
- q_{bl} = total building load (sensible)

Source: ASHRAE Handbook Fundamentals Chapter 17.8

Table 6 Typical Duct Loss/Gain Factors

| Duct Location | Supply/Return Leakage Insulation ft ² ·h·°F/Btu | 1 Story | | | | | | 2 or More Stories | | | | | |
|-------------------|---|---------|------|------|-------|------|------|--------------------------|------|------|-------|------|------|
| | | 11%/11% | | | 5%/5% | | | 11%/11% | | | 5%/5% | | |
| | | R-0 | R-4 | R-8 | R-0 | R-4 | R-8 | R-0 | R-4 | R-8 | R-0 | R-4 | R-8 |
| Conditioned space | | | | | | | | No loss ($F_{dl} = 0$) | | | | | |
| Attic | C | 1.26 | 0.71 | 0.63 | 0.68 | 0.33 | 0.27 | 1.02 | 0.66 | 0.60 | 0.53 | 0.29 | 0.25 |
| | H/F | 0.49 | 0.29 | 0.25 | 0.34 | 0.16 | 0.13 | 0.41 | 0.26 | 0.24 | 0.27 | 0.14 | 0.12 |
| | H/HP | 0.56 | 0.37 | 0.34 | 0.34 | 0.19 | 0.16 | 0.49 | 0.35 | 0.33 | 0.28 | 0.17 | 0.15 |
| Basement | C | 0.12 | 0.09 | 0.09 | 0.07 | 0.05 | 0.04 | 0.11 | 0.09 | 0.09 | 0.06 | 0.04 | 0.04 |
| | H/F | 0.28 | 0.18 | 0.16 | 0.19 | 0.10 | 0.08 | 0.24 | 0.17 | 0.15 | 0.16 | 0.09 | 0.08 |
| | H/HP | 0.23 | 0.17 | 0.16 | 0.14 | 0.09 | 0.08 | 0.20 | 0.16 | 0.15 | 0.12 | 0.08 | 0.07 |
| Crawlspace | C | 0.16 | 0.12 | 0.11 | 0.10 | 0.06 | 0.05 | 0.14 | 0.12 | 0.11 | 0.08 | 0.06 | 0.05 |
| | H/F | 0.49 | 0.29 | 0.25 | 0.34 | 0.16 | 0.13 | 0.41 | 0.26 | 0.24 | 0.27 | 0.14 | 0.12 |
| | H/HP | 0.56 | 0.37 | 0.34 | 0.34 | 0.19 | 0.16 | 0.49 | 0.35 | 0.33 | 0.28 | 0.17 | 0.15 |

Values calculated for ASHRAE *Standard* 152 default duct system surface area using model of Francisco and Palmiter (1999). Values are provided as guidance only; losses can differ substantially for other conditions and configurations. Assumed surrounding temperatures:

Cooling (C): $t_o = 95^\circ\text{F}$, $t_{attic} = 120^\circ\text{F}$, $t_b = 68^\circ\text{F}$, $t_{crawl} = 72^\circ\text{F}$ Heating/furnace (H/F) and heating/heat pump (H/HP): $t_o = 32^\circ\text{F}$, $t_{attic} = 32^\circ\text{F}$, $t_b = 64^\circ\text{F}$, $t_{crawl} = 32^\circ\text{F}$

Source: ASHRAE Handbook Fundamentals 2013, Chapter 17.8

Loads Due to Latent Gains

- Use equation (32):

$$q_l = q_{vi,l} \times q_{ig,l}$$

- Usually added at the end
 - Sometimes as a percentage of total sensible gain, but that is not the preferred method

Source: ASHRAE Handbook Fundamentals 2013, Chapter 17.10

Cooling Load Summary

Table 15 Summary of RLF Cooling Load Equations

| Load Source | Equation | Tables and Notes |
|-----------------------------------|---|--|
| Exterior opaque surfaces | $q_{opq} = A \times CF$ $CF = U(OF_t \Delta t + OF_b + OF_r, DR)$ | OF factors from Table 7 |
| Exterior transparent surfaces | $q_{fen} = A \times CF$ $CF = U(\Delta t - 0.46DR) + PXI \times SHGC \times IAC \times FF_s$ | PXI from Table 9 plus adjustments FF _s from Table 13 |
| Partitions to unconditioned space | $q = AU\Delta t$ | Δt = temperature difference across partition |
| Ventilation/infiltration | $q_s = C_s Q \Delta t$ | See Common Data and Procedures section |
| Occupants and appliances | $q_{ig,s} = 464 + 0.7A_{cf} + 75N_{oc}$ | |
| Distribution | $q_d = F_{dl} \sum q$ | F_{dl} from Table 6 |
| Total sensible load | $q_s = q_d + \sum q$ | |
| Latent load | $q_l = q_{vi,l} + q_{ig,l}$ | |
| Ventilation/infiltration | $q_{vi,l} = C_l Q \Delta W$ | |
| Internal gain | $q_{ig,l} = 68 + 0.07A_{cf} + 41N_{oc}$ | |

Source: ASHRAE Handbook Fundamentals 2013, Chapter 17.11

In Summary

Questions and Discussion

Next Class

- Energy Estimating
 - General considerations
 - Component modeling and loads
 - System modeling
 - Degree-day methods (primarily heating)
 - Bin method (heating & cooling)
- Readings
 - HF Chapter 19.1 to 19.8
 - HF Chapter 19.16 to 19.33

Supplemental Slide

FENESTRATION DIRECT SOLAR, DIFFUSE SOLAR, AND CONDUCTIVE HEAT GAINS

For fenestration heat gain, use the following equations:

Direct beam solar heat gain q_b :

$$q_b = AE_{t,b} \text{SHGC}(\theta) \text{IAC}(\theta, \Omega) \quad (13)$$

Diffuse solar heat gain q_d :

$$q_d = A(E_{t,d} + E_{t,r}) \langle \text{SHGC} \rangle_D \text{IAC}_D \quad (14)$$

Conductive heat gain q_c :

$$q_c = UA(T_{out} - T_{in}) \quad (15)$$

Total fenestration heat gain Q :

$$Q = q_b + q_d + q_c \quad (16)$$

Source: ASHRAE Handbook Fundamentals Chapter 18

Supplemental Slide

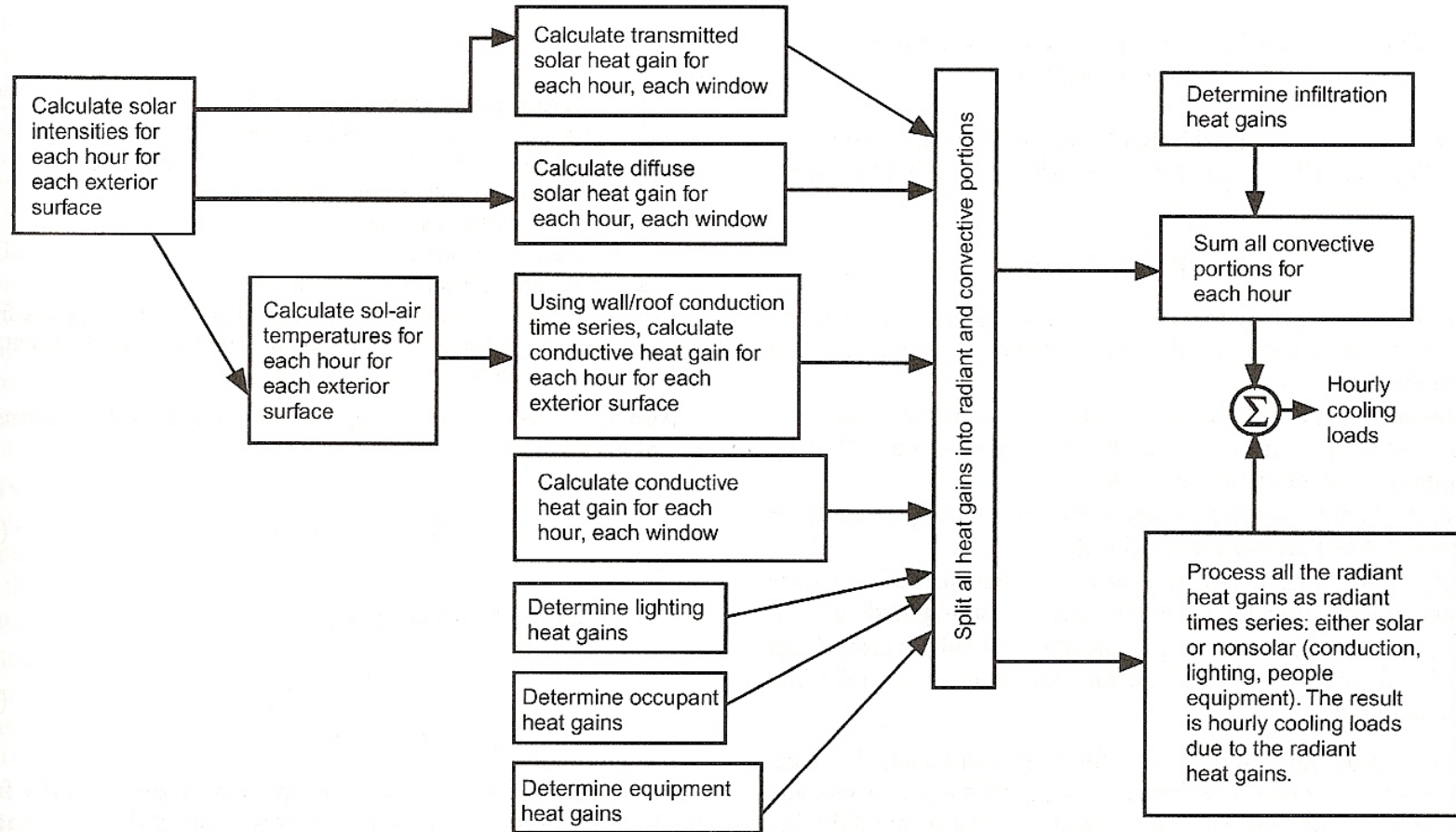


Fig. 8 Overview of Radiant Time Series Method

Source: ASHRAE Handbook Fundamentals Chapter 18

Supplemental Slide

Table 14 Recommended Radiative/Convective Splits for Internal Heat Gains

| Heat Gain Type | Recommended Radiative Fraction | Recommended Convective Fraction | Comments |
|--------------------------------------|--|--|---|
| Occupants, typical office conditions | 0.6 | 0.4 | See Table 1 for other conditions. |
| Equipment | 0.1 to 0.8 | 0.9 to 0.2 | See Tables 6 to 12 for details of equipment heat gain and recommended radiative/convective splits for motors, cooking appliances, laboratory equipment, medical equipment, office equipment, etc. |
| Office, with fan | 0.10 | 0.9 | |
| Without fan | 0.3 | 0.7 | |
| Lighting | | | Varies; see Table 3. |
| Conduction heat gain | | | |
| Through walls and floors | 0.46 | 0.54 | |
| Through roof | 0.60 | 0.40 | |
| Through windows | 0.33 (SHGC > 0.5) 0.46 (SHGC < 0.5) | 0.67 (SHGC > 0.5) 0.54 (SHGC < 0.5) | |
| Solar heat gain through fenestration | | | |
| Without interior shading | 1.0 | 0.0 | Varies; see Tables 13A to 13G in Chapter 15. |
| With interior shading | | | |
| Infiltration | 0.0 | 1.0 | |

Source: Nigusse (2007).

Source: ASHRAE Handbook Fundamentals
Chapter 18

Supplemental Slide

Table 15 Solar Absorptance Values of Various Surfaces

| Surface | Absorptance |
|----------------------------------|--------------|
| Brick, red (Purdue) ^a | 0.63 |
| Paint | |
| Red ^b | 0.63 |
| Black, matte ^b | 0.94 |
| Sandstone ^b | 0.50 |
| White acrylic ^a | 0.26 |
| Sheet metal, galvanized | |
| New ^a | 0.65 |
| Weathered ^a | 0.80 |
| Shingles | 0.82 |
| Gray ^b | |
| Brown ^b | 0.91 |
| Black ^b | 0.97 |
| White ^b | 0.75 |
| Concrete ^{a,c} | 0.60 to 0.83 |

Source: ASHRAE Handbook
Fundamentals
Chapter 18

Supplemental Slide

Table 16 Wall Conduction Time Series (CTS)

| Wall Number = | CURTAIN WALLS | | | STUD WALLS | | | | EIFS | | | BRICK WALLS | | | | | | | | | |
|--|----------------------------|-------|-------|------------|-------|-------|-------|-------|-------|-------|-------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| U-Factor, Btu/h·ft ² ·°F | 0.075 | 0.076 | 0.075 | 0.074 | 0.074 | 0.071 | 0.073 | 0.118 | 0.054 | 0.092 | 0.101 | 0.066 | 0.050 | 0.102 | 0.061 | 0.111 | 0.124 | 0.091 | 0.102 | 0.068 |
| Total R | 13.3 | 13.2 | 13.3 | 13.6 | 13.6 | 14.0 | 13.8 | 8.5 | 18.6 | 10.8 | 9.9 | 15.1 | 20.1 | 9.8 | 16.3 | 9.0 | 8.1 | 11.0 | 9.8 | 14.6 |
| Mass, lb/ft ² | 6.3 | 4.3 | 16.4 | 5.2 | 17.3 | 5.2 | 13.7 | 7.5 | 7.8 | 26.8 | 42.9 | 44.0 | 44.2 | 59.6 | 62.3 | 76.2 | 80.2 | 96.2 | 182.8 | 136.3 |
| Thermal Capacity, Btu/ft ² ·°F | 1.5 | 1.0 | 3.3 | 1.2 | 3.6 | 1.6 | 3.0 | 1.8 | 1.9 | 5.9 | 8.7 | 8.7 | 8.7 | 11.7 | 12.4 | 15.7 | 15.3 | 19.0 | 38.4 | 28.4 |
| Hour | Conduction Time Factors, % | | | | | | | | | | | | | | | | | | | |
| 0 | 18 | 25 | 8 | 19 | 6 | 7 | 5 | 11 | 2 | 1 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 3 | 4 | 3 |
| 1 | 58 | 57 | 45 | 59 | 42 | 44 | 41 | 50 | 25 | 2 | 5 | 4 | 1 | 1 | 2 | 2 | 1 | 3 | 4 | 3 |
| 2 | 20 | 15 | 32 | 18 | 33 | 32 | 34 | 26 | 31 | 6 | 14 | 13 | 7 | 2 | 2 | 2 | 3 | 3 | 4 | 3 |
| 3 | 4 | 3 | 11 | 3 | 13 | 12 | 13 | 9 | 20 | 9 | 17 | 17 | 12 | 5 | 3 | 4 | 6 | 3 | 4 | 4 |
| 4 | 0 | 0 | 3 | 1 | 4 | 4 | 4 | 3 | 11 | 9 | 15 | 15 | 13 | 8 | 5 | 5 | 7 | 3 | 4 | 4 |
| 5 | 0 | 0 | 1 | 0 | 1 | 1 | 2 | 1 | 5 | 9 | 12 | 12 | 13 | 9 | 6 | 6 | 8 | 4 | 4 | 4 |
| 6 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 3 | 8 | 9 | 9 | 11 | 9 | 7 | 6 | 8 | 4 | 4 | 5 |
| 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 7 | 7 | 9 | 9 | 7 | 7 | 8 | 5 | 4 | 5 |
| 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 5 | 5 | 7 | 8 | 7 | 7 | 8 | 5 | 4 | 5 |
| 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 4 | 4 | 6 | 7 | 7 | 6 | 7 | 5 | 4 | 5 |
| 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 3 | 3 | 5 | 7 | 6 | 6 | 6 | 5 | 4 | 5 |
| 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 2 | 2 | 4 | 6 | 6 | 6 | 6 | 5 | 5 | 5 |
| 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 2 | 2 | 3 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 2 | 2 | 4 | 5 | 5 | 4 | 5 | 5 | 5 |
| 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 2 | 2 | 4 | 5 | 5 | 4 | 5 | 5 | 5 |
| 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 1 | 1 | 3 | 4 | 4 | 3 | 5 | 4 | 4 |
| 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 1 | 1 | 3 | 4 | 4 | 3 | 5 | 4 | 4 |
| 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 1 | 2 | 3 | 4 | 3 | 4 | 4 | 4 |
| 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 3 | 3 | 2 | 4 | 4 | 4 |
| 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 3 | 3 | 2 | 4 | 4 | 4 |
| 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 3 | 3 | 2 | 4 | 4 | 4 |
| 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 4 | 4 | 4 |
| 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 4 | 4 | 3 |
| 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 3 |
| Total Percentage | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Layer ID from outside to inside (see Table 18) | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 |
| | F09 | F08 | F10 | F08 | F10 | F11 | F07 | F06 | F06 | F06 | M01 | M01 | M01 | M01 | M01 | M01 | M01 | M01 | M01 | M01 |
| | F04 | F04 | F04 | G03 | G03 | G02 | G03 | I01 | I01 | I01 | F04 | F04 | F04 | F04 | F04 | F04 | F04 | F04 | F04 | F04 |
| | I02 | I02 | I02 | I04 | I04 | I04 | I04 | G03 | G03 | G03 | I01 | G03 | I01 | I01 | M03 | I01 | I01 | I01 | I01 | M15 |
| | F04 | F04 | F04 | G01 | G01 | G04 | G01 | F04 | I04 | M03 | G03 | I04 | G03 | M03 | I04 | M05 | M01 | M13 | M16 | I04 |
| | G01 | G01 | G01 | F02 | F02 | F02 | F02 | G01 | G01 | F04 | F04 | G01 | I04 | F02 | G01 | G01 | F02 | F04 | F04 | G01 |
| | F02 | F02 | F02 | — | — | — | — | F02 | F02 | G01 | G01 | F02 | G01 | — | F02 | F02 | — | G01 | G01 | F02 |
| | — | — | — | — | — | — | — | — | — | F02 | F02 | — | F02 | — | — | — | — | F02 | F02 | — |

Source: ASHRAE Handbook Fundamentals Chapter 18

Supplemental Slide

Table 17 Roof Conduction Time Series (CTS)

| Roof Number | SLOPED FRAME ROOFS | | | | | | WOOD DECK | | METAL DECK ROOFS | | | | | CONCRETE ROOFS | | | | | |
|--|----------------------------|-------|-------|-------|-------|-------|-----------|-------|------------------|-------|-------|-------|-------|----------------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| U-Factor, Btu/h·ft ² ·°F | 0.044 | 0.040 | 0.045 | 0.041 | 0.042 | 0.041 | 0.069 | 0.058 | 0.080 | 0.065 | 0.057 | 0.036 | 0.052 | 0.054 | 0.052 | 0.051 | 0.056 | 0.055 | 0.042 |
| Total R | 22.8 | 25.0 | 22.2 | 24.1 | 23.7 | 24.6 | 14.5 | 17.2 | 12.6 | 15.4 | 17.6 | 27.6 | 19.1 | 18.6 | 19.2 | 19.7 | 18.0 | 18.2 | 23.7 |
| Mass, lb/ft ² | 5.5 | 4.3 | 2.9 | 7.1 | 11.4 | 7.1 | 10.0 | 11.5 | 4.9 | 6.3 | 5.1 | 5.6 | 11.8 | 30.6 | 43.9 | 57.2 | 73.9 | 97.2 | 74.2 |
| Thermal Capacity, Btu/ft ² ·°F | 1.3 | 0.8 | 0.6 | 2.3 | 3.6 | 2.3 | 3.7 | 3.9 | 1.4 | 1.6 | 1.4 | 1.6 | 2.8 | 6.6 | 9.3 | 12.0 | 16.3 | 21.4 | 16.2 |
| Hour | Conduction Time Factors, % | | | | | | | | | | | | | | | | | | |
| 0 | 6 | 10 | 27 | 1 | 1 | 1 | 0 | 1 | 18 | 4 | 8 | 1 | 0 | 1 | 2 | 2 | 2 | 3 | 1 |
| 1 | 45 | 57 | 62 | 17 | 17 | 12 | 7 | 3 | 61 | 41 | 53 | 23 | 10 | 2 | 2 | 2 | 2 | 3 | 2 |
| 2 | 33 | 27 | 10 | 31 | 34 | 25 | 18 | 8 | 18 | 35 | 30 | 38 | 22 | 8 | 3 | 3 | 5 | 3 | 6 |
| 3 | 11 | 5 | 1 | 24 | 25 | 22 | 18 | 10 | 3 | 14 | 7 | 22 | 20 | 11 | 6 | 4 | 6 | 5 | 8 |
| 4 | 3 | 1 | 0 | 14 | 13 | 15 | 15 | 10 | 0 | 4 | 2 | 10 | 14 | 11 | 7 | 5 | 7 | 6 | 8 |
| 5 | 1 | 0 | 0 | 7 | 6 | 10 | 11 | 9 | 0 | 1 | 0 | 4 | 10 | 10 | 8 | 6 | 7 | 6 | 8 |
| 6 | 1 | 0 | 0 | 4 | 3 | 6 | 8 | 8 | 0 | 1 | 0 | 2 | 7 | 9 | 8 | 6 | 6 | 6 | 7 |
| 7 | 0 | 0 | 0 | 2 | 1 | 4 | 6 | 7 | 0 | 0 | 0 | 0 | 5 | 7 | 7 | 6 | 6 | 6 | 7 |
| 8 | 0 | 0 | 0 | 0 | 0 | 2 | 5 | 6 | 0 | 0 | 0 | 0 | 4 | 6 | 7 | 6 | 6 | 6 | 6 |
| 9 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 5 | 0 | 0 | 0 | 0 | 3 | 5 | 6 | 6 | 5 | 5 | 5 |
| 10 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 5 | 0 | 0 | 0 | 0 | 2 | 5 | 5 | 6 | 5 | 5 | 5 |
| 11 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 4 | 0 | 0 | 0 | 0 | 1 | 4 | 5 | 5 | 5 | 5 | 5 |
| 12 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 1 | 3 | 5 | 5 | 4 | 5 | 4 |
| 13 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 1 | 3 | 4 | 5 | 4 | 4 | 4 |
| 14 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 4 | 4 | 4 | 3 |
| 15 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 4 | 4 | 4 | 3 |
| 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 4 | 3 | 4 | 3 |
| 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 4 | 3 | 4 | 3 |
| 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 3 | 3 | 3 | 2 |
| 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 3 | 3 | 2 |
| 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 3 | 3 | 2 |
| 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 3 | 3 | 2 |
| 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 2 | 2 | 2 |
| 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 2 | 2 |
| | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Layer ID from outside to inside (see Table 18) | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 | F01 |
| | F08 | F08 | F08 | F12 | F14 | F15 | F13 | F13 | F13 | F13 | F13 | F13 | M17 | F13 | F13 | F13 | F13 | F13 | F13 |
| | G03 | G03 | G03 | G05 | G05 | G05 | G03 | G03 | G03 | G03 | G03 | G03 | F13 | G03 | G03 | G03 | G03 | G03 | M14 |
| | F05 | F05 | F05 | F05 | F05 | F05 | I02 | I02 | I02 | I02 | I03 | I02 | G03 | I03 | I03 | I03 | I03 | I03 | F05 |
| | I05 | I05 | I05 | I05 | I05 | I05 | G06 | G06 | F08 | F08 | F08 | I03 | I03 | M11 | M12 | M13 | M14 | M15 | I05 |
| | G01 | F05 | F03 | F05 | F05 | F05 | F03 | F05 | F03 | F05 | F03 | F08 | F08 | F03 | F03 | F03 | F03 | F03 | F16 |
| | F03 | F16 | — | G01 | G01 | G01 | — | F16 | — | F16 | — | — | F03 | — | — | — | — | — | F03 |
| | — | F03 | — | F03 | F03 | F03 | — | F03 | — | F03 | — | — | — | — | — | — | — | — | — |

Source: ASHRAE Handbook Fundamentals Chapter 18

Supplemental Slide

Table 30 Window Component of Cooling Load (No Blinds or Overhang)

| Local Standard Hour | Unshaded Direct Beam Solar (if AC = 1) | | | | | | Shaded Direct Beam (AC < 1.0) + Diffuse + Conduction | | | | | | | | | Window Cooling Load, Btu/h |
|---------------------|--|----------------------|---------------------|---------------------------|---------------|---------------------|--|--------------------------|-----------------------------|------------------------|-----------------------|--------------------|----------------------------|---------------|---------------------|----------------------------|
| | Beam Heat Gain, Btu/h | Convective 0%, Btu/h | Radiant 100%, Btu/h | Solar RTS, Zone Type 8, % | Radiant Btu/h | Cooling Load, Btu/h | Beam Heat Gain, Btu/h | Diffuse Heat Gain, Btu/h | Conduction Heat Gain, Btu/h | Total Heat Gain, Btu/h | Convective 54%, Btu/h | Radiant 46%, Btu/h | Non-solar RTS, Zone Type 8 | Radiant Btu/h | Cooling Load, Btu/h | |
| 1 | 0 | 0 | 0 | 54 | 196 | 196 | 0 | 0 | -54 | -54 | -29 | -25 | 49 | 138 | 109 | 305 |
| 2 | 0 | 0 | 0 | 16 | 196 | 196 | 0 | 0 | -90 | -90 | -48 | -41 | 17 | 118 | 70 | 266 |
| 3 | 0 | 0 | 0 | 8 | 196 | 196 | 0 | 0 | -121 | -121 | -65 | -56 | 9 | 101 | 36 | 232 |
| 4 | 0 | 0 | 0 | 4 | 196 | 196 | 0 | 0 | -148 | -148 | -80 | -68 | 5 | 84 | 4 | 200 |
| 5 | 0 | 0 | 0 | 3 | 196 | 196 | 0 | 0 | -166 | -166 | -90 | -76 | 3 | 67 | -23 | 174 |
| 6 | 0 | 0 | 0 | 2 | 196 | 196 | 0 | 106 | -148 | -42 | -23 | -19 | 2 | 81 | 58 | 254 |
| 7 | 0 | 0 | 0 | 1 | 196 | 196 | 0 | 569 | -81 | 488 | 263 | 224 | 2 | 196 | 460 | 656 |
| 8 | 0 | 0 | 0 | 1 | 191 | 191 | 0 | 1002 | 76 | 1078 | 582 | 496 | 1 | 361 | 943 | 1134 |
| 9 | 0 | 0 | 0 | 1 | 169 | 169 | 0 | 1371 | 251 | 1622 | 876 | 746 | 1 | 539 | 1415 | 1583 |
| 10 | 0 | 0 | 0 | 1 | 132 | 132 | 0 | 1665 | 408 | 2073 | 1119 | 953 | 1 | 705 | 1824 | 1956 |
| 11 | 0 | 0 | 0 | 1 | 86 | 86 | 0 | 1887 | 547 | 2434 | 1314 | 1119 | 1 | 849 | 2164 | 2249 |
| 12 | 0 | 0 | 0 | 1 | 42 | 42 | 0 | 2177 | 641 | 2818 | 1522 | 1296 | 1 | 994 | 2516 | 2558 |
| 13 | 537 | 0 | 537 | 1 | 300 | 300 | 0 | 2436 | 717 | 3153 | 1703 | 1450 | 1 | 1130 | 2833 | 3133 |
| 14 | 2183 | 0 | 2183 | 1 | 1265 | 1265 | 0 | 2614 | 762 | 3376 | 1823 | 1553 | 1 | 1241 | 3064 | 4329 |
| 15 | 3722 | 0 | 3722 | 1 | 2402 | 2402 | 0 | 2648 | 762 | 3410 | 1841 | 1569 | 1 | 1303 | 3144 | 5547 |
| 16 | 4583 | 0 | 4583 | 1 | 3266 | 3266 | 0 | 2479 | 708 | 3187 | 1721 | 1466 | 1 | 1291 | 3012 | 6278 |
| 17 | 4392 | 0 | 4392 | 1 | 3506 | 3506 | 0 | 2072 | 632 | 2703 | 1460 | 1243 | 1 | 1191 | 2651 | 6157 |
| 18 | 3177 | 0 | 3177 | 1 | 3010 | 3010 | 0 | 1429 | 538 | 1967 | 1062 | 905 | 1 | 999 | 2061 | 5071 |
| 19 | 1017 | 0 | 1017 | 1 | 1753 | 1753 | 0 | 599 | 399 | 998 | 539 | 459 | 1 | 717 | 1256 | 3008 |
| 20 | 0 | 0 | 0 | 0 | 832 | 832 | 0 | 0 | 300 | 300 | 162 | 138 | 1 | 456 | 618 | 1449 |
| 21 | 0 | 0 | 0 | 0 | 496 | 496 | 0 | 0 | 215 | 215 | 116 | 99 | 0 | 332 | 448 | 945 |
| 22 | 0 | 0 | 0 | 0 | 334 | 334 | 0 | 0 | 130 | 130 | 70 | 60 | 0 | 255 | 325 | 659 |
| 23 | 0 | 0 | 0 | 0 | 248 | 248 | 0 | 0 | 58 | 58 | 31 | 27 | 0 | 203 | 234 | 483 |
| 24 | 0 | 0 | 0 | 0 | 206 | 206 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 167 | 167 | 373 |

Source: ASHRAE Handbook Fundamentals Chapter 18